

# **Technical Note**

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# Helicopter Noise and the Acoustic Design of the Building Envelope

### 1 Introduction

Sweco UK Ltd have been commissioned to undertake a desk-based assessment to determine the noise impacts on the surrounding new and proposed buildings of the new helipad proposed to be located on the top of Building B at Västerviks sjukhus.

This technical note sets out the findings of the desk-based assessment.

## 2 Desk Based Study

### 2.1 Background

The development of Västerviks sjukhus proposes the construction of new buildings and the location of a new helipad on top of Building B.

It is understood that the use of the proposed helipad will be occasional and for the purposes of this study, helicopter movements are assumed to occur two times during the daytime (07:00-23:00) and two times during the night-time period (23:00-07:00).

The room uses for the buildings have not been specified as part of this assessment. The new proposed layout of Västerviks sjukhus is shown in Figure 1.

The labelling of the results follows the convention indicated in Figure 1.

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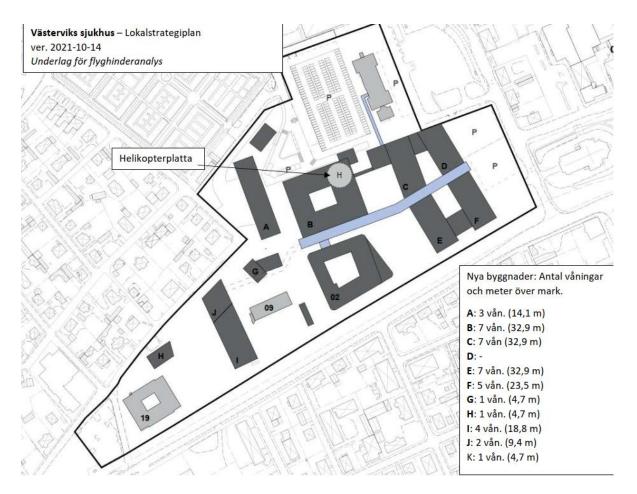


Figure 1: Building B and the proposed helipad.

#### 2.1.1 Indoor Noise Levels Targets

As room uses within the buildings are unclear, indoor noise level targets have been defined considering the potential effects that could occur due to helicopter noise and are shown in Table 1. It is noted that these indoor noise level criteria apply only where helicopter movements are occasional – lower indoor noise targets would be appropriate where more helicopter movements occur.

Table 1: Recomn	nended indoor noise targ	gets assuming helicopter	r movements are occasional
Lype of room	Potential effects due to	Recommended indoor helicopter noise level target	Justification
	Disruption of rest and/or sleep, annoyance.	with a target of ≤55 dB L <sub>AFmax,event</sub> where feasible.	Aircraft noise and sleep research indicates that aircraft events resulting in indoor maximum sound levels of <65 dB L <sub>AFmax,event</sub> are not likely to result in awakenings that can be recalled. Awakenings due to sound of this



Table 1: Recomn	nended indoor noise targ	ets assuming helicopter	r movements are occasional
Type of room	Potential effects due to	Recommended indoor helicopter noise level target	Justification
			level were indistinguishable from spontaneous awakenings.
consultation rooms,	communication, interference with activities requiring	Limit of ≤60 dB L <sub>AFmax,event</sub> with a target of ≤55 dB L <sub>AFmax,event</sub> where feasible	It is good practice to apply indoor noise of 50 to 55 dB $L_{AFmax, event}$ for regular events. A relaxation of 5 to 10 dB is considered appropriate given the occasional nature of helicopter movements.
(ancillary rooms that are not	Interference with speech communication, masking of sound from important sources (such as alarms)	≤70 dB L <sub>AFmax,event</sub>	Considered sufficient to avoid masking of alarms, but likely to require occupants to raise voices/shout above the sound of the helicopter

## 3 Assessment Approach

A sound propagation model of Västerviks sjukhus, the helipad, and the surrounding area has been created in order to evaluate maximum sound pressure levels during helicopter movements. This three-dimensional model was constructed using the Datakustik Cadna/A sound propagation modelling software. The software carries out sound propagation predictions in accordance with ISO 9613-2 '*Acoustics – Attenuation of sound during propagation outdoors – Part 2: General method of calculation*' (1996).

The model has been used to estimate the maximum sound pressure level from the helicopter along any point of the flightpath at each part of the building. In reality the maximum sound pressure level will vary, depending on the flight direction of the helicopter.

The following assumptions were incorporated into the assessment.

- Initially, the worst case noise output shown in Table 2 was used within the model.
- The maximum sound pressure level was then predicted considering helicopter arrivals/departures on any of the four routes shown in Figure 2.
- The helicopter movement was represented by point sources along the flightpath corridor spaced 50 metres apart, as shown in **Error! Reference source not found.**.
- The predicted sound pressure levels outside the building are facade levels and include second order reflections from surrounding buildings.

Table 2: Sound powe	er levels	of heli	copters							
Helicopter Type	Assum	ed soun	d power	level of	helicopt	er [dB L	"], per o	ctave ba	ind [Hz]	A-weighted
	31.5	63	125	250	500	1000	2000	4000	8000	sound power level [dB L <sub>wA</sub> ]
Worst-case helicopter	141	137	133	133	134	130	125	116	104	135
EC-145	131	132	130	131	132	128	123	113	112	133
"Twin Squirrel"	-	132	131	135	132	129	125	118	122	133



AW-169 (fly-over)	144	135	134	131	131	127	121	114	94	132

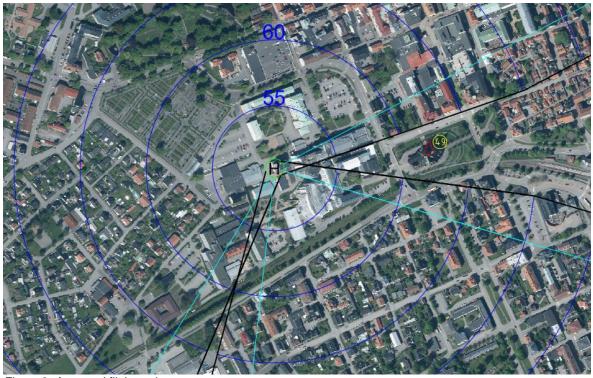


Figure 2: Assumed flight-paths

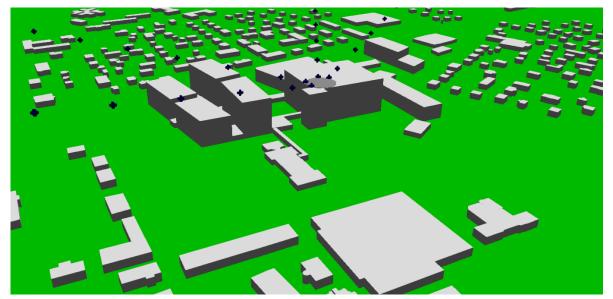


Figure 3: Sound propagation model



## 4 Outdoor Noise Level Predictions: Worst-Case Helicopter

Predicted outdoor maximum sound pressure levels during the worst-case helicopter movement outside Building B are shown in **Error! Reference source not found.4**.

Row Labels	2	3	4	5	6	7	8	24	25	26	27	28	29	16	17	18	19	20	21	22	23	9	10	11	12	13	14	15
Floor		dB L	AFMa	at No	orth Fa	içade			dB L	AFMax	at East	Façade				B LAF	Max at	South	Façade	2			dB	LAFM	ax at V	Vest F	açade	
Level 10	84	82	84	83	83	82	2 81	98	100	102	102	102	103	98	96	99	104	105	100	96	93	91	92	94	95	98	100	103
Level 9	80	78	77	78	77	78	3 77	97	100	101	102	100	100	98	95	99	102	103	99	96	93	91	92	93	95	97	100	102
Level 8	78	77	76	75	76	76	5 76	97	99	101	101	100	100	97	95	96	99	100	97	94	92	91	92	93	95	97	99	101
Level 7	76	76	76	75	74	74	1 75	97	99	100	100	99	99	96	94	95	97	97	95	93	91	90	92	93	95	96	98	100
Level 6	75	76	75	74	74	72	2 72	96	98	99	99	98	99	95	93	93	95	95	93	91	90	90	92	93	94	96	97	99
Level 5	74	75	75	74	73	72	2 72	96	97	98	99	98	98	94	93	92	93	93	92	90	90	90	91	93	94	95	97	98
Level 4	- 74	75	74	74	72	72	2 71	96	97	98	98	97	97	94	92	91	92	92	91	90	90	90	91	92	94	95	96	97
Level 3	73	74	74	73	72	71	l 71	95	96	97	97	97	97	93	92	91	91	91	90	89	90	90	91	92	93	95	96	96
Level 2	73	73	73	73	72	71	l 71	95	96	96	96	96	96	92	91	90	90	90	89	89	90	90	91	92	93	94	95	96
Level 1	72	73	73	72	71	71	l 71	94	95	96	96	95	96	92	91	90	89	89	88	89	90	90	91	92	93	94	94	95
Level 0	72	72	72	72	71	71	71	94	95	95	95	95	95									89	90	91	92	93	94	94

Figure 4: Outdoor maximum sound pressure levels during worst-case helicopter movement (Building B)

The predicted outdoor maximum noise level for the nearest buildings to Building B are displayed in the figures below.

Façade Position	1	2	3	4	5	6	7	8	37	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	4	25	26	27	28 2	9 30	31	32 33	3 34	35	36
Floor			dB LA	FMax	at N	orth Fa	açade					dB LAF	Max a	at East F	açade	5					dB L	AFMa	x at W	est Fag	ade					dB	LAFN	lax at S	outh F	açade	
Level 10	96	95	97	98	97	96	94	1 94	97		9 8	87	8	5 86	85	85	88	88	88	89	90	92	93	95	97	99	99	100	99 9	7 95	94	96 9	8 100	0 100	100
Level 9	95	95	96	98	97	95	94	l 94	97	8	8 8	7 86	8	5 86	85	85	88	88	88	89	90	92	93	95	97	98	98	99	98 9	7 95	93	95 9	8 99	9 100	100
Level 8	95	94	96	97	96	95	94	93	96	8	8 8	86	8	5 86	85	85	87	88	88	89	90	91	93	95	96	97	98	98	97 9	6 94	93	95 9	7 9!	9 99	99
Level 7	94	94	95	96	96	94	93	93	95	8	8 8	7 86	8	5 85	85	85	87	88	88	89	90	91	93	94	96	97	97	97	97 9	6 94	93	95 9	7 98	8 98	3 98
Level 6	94	93	95	95	95	94	93	93	95	8	8 8	86	8	5 85	85	85	87	87	88	89	90	91	92	94	95	96	96	96	96 9	5 94	93	94 9	6 9°	7 98	3 98
Level 5	93	93	94	95	94	93	93	92	94	- 8	8 8	86	8	5 85	85	85	87	87	88	89	90	91	92	93	95	95	96	96	95 9	5 93	93	94 9	6 9	7 97	7 97
Level 4	93	92	94	94	94	93	92	2 92	93	8	8 8	86	8	5 85	85	85	87	87	88	89	90	91	92	93	94	95	95	95	95 9	4 93	92	94 9	5 96	5 96	i 96
Level 3	92	92	93	93	93	92	92	91	93	8	8 8	86	8	5 85	85	85	87	87	88	88	89	90	92	93	94	94	94	95	94 9	4 93	92	93 9	5 95	5 96	i 96
Level 2	92	92	92	93	93	92	91	91	92	8	8 8	7 86	8	5 85	84	84	87	87	88	88	89	90	91	92	93	94	94	94	94 9	3 92	92	93 9	4 95	5 95	i 95
Level 1	91	91	92	92	92	91	91	91	92	8	7 8	7 86	8	5 84	84	84	87	87	87	88	89	90	91	92	93	93	93	93	93 9	3 92	91	93 9	4 94	4 94	4 95
Level 0	91		91	92	91	91	90	90	91	8	7 8	5 86	8	5 84	84	83	87	87	87	88	89	90	91	92	92	93	93	93	93 9	2 91	91	92 9	3 94	4 94	1 94

Figure 5: Outdoor maximum sound pressure levels during worst-case helicopter movement (Building 02)

Façade Position	1	2	3	4	5	6	7	,	8	9	10	11	12	13		14	15	16	17	18	19	20	21	22	23	24
							П								dB L	AFMa	ax at									
Floor	dl	BLAFN	/lax at	Nort	th Faça	ade			dB L	AFMax	at East	Façade			Sou	th Fag	ade			dB	LAFMa	ax at V	Vest F	açade		
Level 4	78	78	79	8	6 8	7 88		89	90	91	93	94	96		96	95	94	9	0 8	9 87	7 86	85	84	83	82	8
Level 3	73	74	79	8	6 8	7 88		89	90	91	93	94	95		95	95	94	8	8 8	7 86	5 85	84	83	83	82	8
Level 2	72	74	79	8	6 8	7 88		89	90	91	92	93	95		95	94	93	8	7 8	5 85	5 85	84	83	83	82	8
Level 1	72	74	79	8	6 8	7 88		89	90	91	92	93	94		94	94	93	8	7 8	5 85	5 84	84	83	83	82	8
Level 0	71	74	78	8	6 8	7 88		89	90	91	92	93	94		94	93	93	8	7 8	5 85	5 84	83	83	82	82	8

Figure 6: Outdoor maximum sound pressure levels during worst-case helicopter movement (Building A)

Façade Position	16	17	18	1	2	3	4	5	6	7		8	9	10	11	12	13	14	15
	dB I	AFMa	ix at							Т	dB L	AFMa	x at						
Floor	Nor	th Faç	ade	0	B LAF	Max a	t East	Façad	e		Sou	th Faç	ade		dB LAF	Max a	t West	Façad	le
Level 7	94	93	91	89	90	91	92	94	95		95	95	94	9	94 9	5 96	95	93	92
Level 6	94	93	91	89	90	91	92	93	94		95	94	93		94 94	4 95	94	93	91
Level 5	94	92	91	89	90	91	92	93	94		94	94	93		93 94	4 94	93	92	91
Level 4	93	92	91	89	89	90	91	93	93		94	93	92		92 9	3 93	93	92	90
Level 3	93	92	91	88	89	90	91	92	93		93	93	92		92 93	2 92	92	91	90
Level 2	93	92	90	88	89	90	91	92	93		93	92	92		91 92	2 91	91	91	90
Level 1	92	91	90	88	89	90	91	91	92		92	92	91		91 9	1 90	91	90	89
Level 0				88	89	89	90	91	92		92	92	91		34		90	90	89

Figure 7: Outdoor maximum sound pressure levels during worst-case helicopter movement (Building F)



Façade Position	10	11	12	4	5	6	7	8	9	1	2	3	13	14	15	16	17	18
	dB l	AFMa	ix at							dB L	AFMa	x at						
Floor	Nor	th Faç	ade	C	B LAF	Max a	t East	Façad	e	Sout	th Faç	ade	d	IB LAFI	Max at	t West	: Façac	le
Level 10	102	99	96	89	91	93	96	102	105	103	104	103	97	96	98	99	98	97
Level 9	100	98	95	89	91	93	95	101	104	101	103	102	97	96	98	99	98	96
Level 8	98	97	95	89	91	93	95	100	102	100	101	101	96	96	98	98	98	96
Level 7	94	95	94	89	91	92	94	99	101	99	100	100	96	95	97	98	97	96
Level 6	92	91	92	89	90	92	94	98	100	99	99	99	95	95	97	97	97	96
Level 5	95	94	93	89	90	92	93	98	99	98	98	98	94	94	97	97	96	95
Level 4	94	93	92	88	90	91	93	97	98	97	97	97	94	94	96	96	96	95
Level 3	93	92	91	88	89	91	92	96	97	96	97	96	93	93	96	96	95	95
Level 2	92	91	90	88	89	90	92	96	96	96	96	96	93	92	95	95	95	94
Level 1	92	90	89	88	89	90	91	95	95	95	95	95	92	92	95	95	95	94
Level 0	91	90	89	88	89	90	90								94	94	94	93

Figure 8: Outdoor maximum sound pressure levels during worst-case helicopter movement (Building C)

Façade Position	7	8	9	10	11	12	13	14		15	16	17	1	2	3	4	5	6
	dB l	AFMa	x at						Τ	dB L	AFMa	x at						
Floor	Nor	th Faç	ade	dB	LAFMa	ix at E	ast Fag	ade		Sou	th Faç	ade	d	B LAFI	Vax at	West	Façad	le
Level 7	96	95	97	97	96	95	93	92		91	93	94	92	91	92	94	99	100
Level 6	95	95	96	97	96	95	93	92		91	92	94	91	91	92	93	98	99
Level 5	95	94	95	96	95	94	93	92		91	92	93	91	90	91	93	97	98
Level 4	94	94	95	95	95	94	93	91		91	92	93	91	90	91	92	97	97
Level 3	93	93	94	95	94	93	92	91		91	92	93	90	89	91	92	96	97
Level 2	93	93	94	94	94	93	92	91		90	91	93	90	89	90	91	95	96
Level 1	92	93	93	94	93	92	92	91		90	91	92	90	89	90	91	95	95
Level 0	91	92	93	93	93	92	91	90	Τ				89	89	90	85		

Figure 9: Outdoor maximum sound pressure levels during worst-case helicopter movement (Building D)

Façade Position	16	17	18	1	2		3	4	5	6		7	8	9	10	11	12	13	14	15
						Π	dB	LAFM	ax at E	ast	Τ	dB L	AFMa	x at						
Floor	dB L/	<b>\FMax</b>	at No	rth Fa	çade			Faç	ade			Sout	th Faç	ade	d	IB LAFI	Max at	: West	Façad	le
Level 10	103	106	104	92	93		95	95	95	94		90	89	88	84	85	86	87	88	90
Level 9	102	104	102	91	93		94	95	95	94		90	89	88	84	85	86	87	88	90
Level 8	101	102	101	91	92		94	94	94	93		90	89	88	84	85	86	87	88	90
Level 7	100	101	100	91	92		93	94	93	93		90	89	88	84	85	86	87	88	90
Level 6	99	100	99	90	92		92	93	93	92		90	89	88	84	85	86	87	88	89
Level 5	98	99	98	90	91		92	92	92	92	Ι	90	89	88	84	85	86	87	88	89
Level 4	97	98	97	90	91		91	92	92	91		89	89	88	84	85	86	87	88	89
Level 3	96	97	97	89	90		91	91	91	91	Ι	89	88	88	84	85	86	87	88	89
Level 2	96	96	96	89	90		90	91	91	90		89	88	88	84	85	85	86	88	89
Level 1	95	95	95	89	89		90	90	90	90		89	88	87	84	84	85	86	87	88
Level 0				88	89		90			89		89	88	87	84	84	85	86	87	88

Figure 10: Outdoor maximum sound pressure levels during worst-case helicopter movement (Building E)

These values allow for a helicopter movement along any point of each flightpath. In reality the maximum sound pressure level will vary with event, depending on the flight direction of the helicopter.



### 5 Assessment of Noise Ingress

#### 5.1 Methodology and Assumptions

Noise ingress calculations have been carried out through applying the approach with ISO 12354-3:2017: *Building acoustics* — *Estimation of acoustic performance of buildings from the performance of elements* — *Part 3: Airborne sound insulation against outdoor sound.* The assessment has considered the worst affected point on the worst affected façade of Buildings B and 02 on floors 10, 8 and 6, and on Buildings D and F on floors 7 and 5.

The following assumptions were incorporated into the assessment for the purposes of this initial study:

- The room is assumed to be reasonably small (4 m by 4 m by 2.8 m).
- The building envelope is assumed to contain two windows (total area of 4.4 m<sup>2</sup>), and it is assumed that these are triple glazed systems with a very stringent sound insulation requirement. The type of glazing under consideration is shown in Appendix A.
- The room is assumed to be ventilated mechanically with no passive vents within the building envelope (and any ductwork opening to outdoors attenuated sufficiently so that it is not an important noise ingress route).
- The room is assumed to include a suspended ceiling system that achieves sound absorption class A over at 80% of the ceiling area, and it is assumed that a reverberation time criterion of 0.6 seconds T<sub>mf</sub> is achieved within sensitive rooms.
- It is assumed that back of house rooms of the same size will have a reverberation time of around 1 second  $T_{\rm mf}.$

The effect of varying the construction of the non-glazed elements within the building enveloped has been investigated. This included consideration of the façade systems shown in Table 3.

In addition to these systems, a comparison with a simple Brick/Block with cavity wall (as seen in Table E1.A of British Standard 8233:2014) has been made. This additional system considers the potential construction of already constructed buildings that are remaining on site.



Table 3: Façade systems considered						
Type of Façade System	Construction	Construction details				
Heavy masonry system	Age is m	200 mm pre-cast concrete, cavity of 150 mm depth containing 150 mm depth of mineral wool insulation (min. 22 kg/m <sup>3</sup> ), 102 mm concrete layer. Point connections between masonry layers spaced every 600 mm.				
Lightweight façade system with rigid connections		25 mm fibre cement panel (40 kg/m²), cavity of 350 mm depth containing 300 mm depth of mineral wool insulation (min. 22 kg/m³), 2 layers of 15 mm acoustic plasterboard (12.6 kg/m² per layer). Both layers supported on steel studwork (max gauge 1.6 mm) with studworks spaced every 600 mm.				
Lightweight façade system with resilient connections and additional dense boards		25 mm fibre cement panel (40 kg/m <sup>2</sup> ), cavity of 350 mm depth containing 300 mm depth of mineral wool insulation (min. 22 kg/m <sup>3</sup> ), 2 layers of 18 mm dense cementitious board (22.9 kg/m <sup>2</sup> per layer), cavity of 63 mm with 60 mm depth of mineral wool insulation (min. 22 kg/m <sup>3</sup> ), 1 layer of 15 mm acoustic plasterboard (12.6 kg/m <sup>2</sup> per layer). Fibre cement and cementitious board supported on steel studwork (max gauge 1.6 mm) with studworks spaced every 600 mm. Additional acoustic plasterboard layer supported on narrow studwork with a resilient rail connection.				

### 5.2 Predicted Indoor Levels

Based on the above assumptions, estimated indoor helicopter noise levels based on the predicted worst-case helicopter noise levels (Table 2) are shown in Tables 4 and 5 below.



Table 4: Estimated indoor maximum sound levels, Brick/Block construction with cavity wall					
Building	Floor	Predicted External Noise Level (dBA L <sub>AF,Max,event</sub> )	Predicted Internal Noise Level (dBA)		
В	10	105	60		
В	8	101	57		
В	6	99	55		
02	10	101	57		
02	8	100	56		
02	6	99	55		
D	7	100	56		
D	5	98	54		
F	7	97	53		
F	5	95	50		

Table 5: Estimated indoor maximum sound levels, lightweight façade system with rigid connections						
Building	Floor	Predicted External Noise Level (dBA L <sub>AF,Max,event</sub> )	Predicted Internal Noise Level (dBA)			
В	10	105	59			
В	8	101	55			
В	6	99	54			
02	10	101	56			
02	8	100	54			
02	6	99	53			
D	7	100	54			
D	5	98	52			
F	7	97	51			
F	5	95	49			

The above results demonstrate the following:

- There is only marginal difference between the façade types considered. This is due to the fact that, even with a triple glazed system, the glazing remains the dominant noise ingress path. This accounts for the expected frequency characteristics of helicopter noise with a moderate to high level of low-frequency sound.
- With a façade that has a minimum  $R_w$  of at least 50dB, plus the triple glazing system, the indoor noise level targets are likely to be achieved at the floors closest to the



helipad when considering "typical" helicopter movements that vary with direction of approach and also helicopter type.

• Within the lower floors, the indoor target of 55 dB L<sub>AFmax,event</sub> is achievable.

It is noted that for all of the above predictions, the sound insulation performance of the building envelope at low frequency (i.e. the 63 Hz octave band) is very important. Unfortunately, the level of uncertainty within the source data, sound insulation data and sound absorption data at low frequency is also greater. This uncertainty can be reduced by ensuring that the acoustic performance of elements at low frequency is tested, using a representative sample element with the same construction and geometry that will be used within the building.

#### 5.3 Outline Façade Sound Insulation Specification

Based on above assessment, it is recommended that the following outline sound insulation requirements for the building envelope is incorporated into the building specifications.

Table 6: Outline sound insulation specification for external glazing							
Minimum s	Minimum sound reduction index of triple glazing system [dB R], per octave band [Hz]						Single-figure sound insulation rating
63	125	250	500	1000	2000	4000	[dB R <sub>w</sub> + C <sub>tr</sub> )]
23	33	41	47	54	57	54	45

Nominal suitable construction:

Triple glazed system. Nominal construction of 8.8 mm laminated glass, 175 mm cavity, 4 mm glass, 16 mm cavity, 6 mm glass.

Table 7: Outline sound insulation specification for the external facade							
Minimum sound reduction index of the external façade [dB R], per octave band [Hz]						Single-figure sound insulation rating	
63	125	250	500	1000	2000	4000	$[dB R_w + C_{tr}]$
34	40	46	52	53	57	61	50

Nominal suitable construction:

Achievable with the lightweight façade system with rigid connections shown in Table 3, subject to the provision of an additional layer of acoustic plasterboard on the inner face. Achievable with the heavy masonry construction as shown in Table 3.

### 6 Conclusion

Prediction of noise levels from the proposed helicopter landing pad at Västerviks sjukhus was undertaken in order to determine potential noise implications within the hospital building. The predicted noise levels were then compared against façade constructions and internal noise levels calculated, which were then compared against the limit levels set out in Table 1.

Based on the assumptions made within the memo, and the constructions detailed in Table 6 and Table 7, the internal noise levels within rooms on the worst affected floors and facades should still meet the limit levels with the occasional use of the helicopter landing pad.